REINFORCED CONCRETE LIGHT MANUFACTURING BUILDING

BY

C. R. LEIBRANDT

ARMOUR INSTITUTE OF TECHNOLOGY

1913

DESIGNS and PLANS

for

A Four Story Reinforced Concrete Light Manufacturing Building

100'-0" x 150'-0"

A Thesis

presented by

Charles Raymond Leibrandt

to the

President and Faculty

of

Armour Institute of Technology

for the degree of

Bachelor of Science in Civil Engineering

having completed the prescribed course

May 1913.

Approved:

Alfred E. Phillips
Prof. of Civil Engineering

H. M. Raymond
Dean of Eng. Studies

L. C. Morrow
Dean of Cult. Studies

Design of four story and basement reinforced concrete building of Class One of Chicago Building Ordinance.

DATA:

Proposed building to be constructed of reinforced concrete skeleton and vitified brick curtain wall.

Span of Floor Beam	20'-0"
" " " Girder	I6'-8"
" " " Slab	8'-4"
Live Load on Floor	I00#/□'
" " " Roof	25#/□'
Weight of Roofing Composition	7#/□'
" " Concrete I - 2 - 4	I50# cu.ft.

STRESSES:

Unit Shearing Stress plain concrete	40#/□"
" Tensile " steel "	I5000#/□"
" Shearing " " "	I2000#/□"
" Complete " reinforced concrete	700#/□"
Allowable Compression Stress plain concrete	400#/□"
" Bond "	70#/□"
" Pressure on soil	5000#/□"

ROOF SLAB.

End Slab.

Live Load	25# sq.ft.
Roofing Composition	7 " "
3" Slab	37.5 " "
Total Load	69.5# sq.ft.

$$M = \frac{W L^2}{I0} = \frac{69.5 \times \overline{8.33}^2 \times I2}{I0} = 5800"\#$$

$$d^2 = \frac{M \times 6}{f_c \times b} = \frac{5800 \times 6}{600 \times I2} = 4.83 \qquad d = 2.2" \qquad \text{Use 3" slab.}$$

$$A = \frac{M}{f_s\, jd} \quad - \quad \text{Effective depth} = 3 - 3/4 = 2\text{-}I/4"$$

$$A = \frac{5800}{I5000 \times .875 \times 2.25} = .I97^{\square}"$$

Use 3/8" round rods, spacing 6", area $2.2^{\square}"$.

$$V = \frac{8.33 \times 69.5}{2} = 290\# \qquad V' = \frac{290}{3 \times I2} = 8.05\#^{\square}" \qquad 40\# \text{ allowable}$$

$$U = \frac{V}{\Sigma o\, jd} = \frac{290}{(I2 \times I.I8) \times .875 \times 2.25} = 62.5\#^{\square}" \qquad 70\# \text{ allowable}$$

Intermediate Slab.

Same thickness as end slab.

$$M = \frac{W L^2}{I2} = \frac{69.5 \times \overline{8.33}^2 \times I2}{I2} = 4830"\#$$

$$A = \frac{4830}{I5000 \times .875 \times 2.25} = .I7\#^{\square}"$$

Use 3/8" round rods, spacing 6" to take care of bond stress.

ROOF BEAM.

End Beam Span 20' 0"

$$M = \frac{W\ b\ L^2}{10} = \frac{69.5 \times 8.33 \times \overline{20}^2 \times 12}{10} = 278000"\#$$

B.M. due to weight of beam $= \frac{12.5 \times 6}{144} \times \frac{150 \times 20 \times 12}{8} = 47000"\#$

Total M = 278000 + 47000 = 325000"#

$$V = \frac{20 \times 8.33 \times 69.5}{2} = 5800\#$$

$$U = 100\#^{a}" \qquad \frac{5800}{100} = 58$$

$$db = 58 \qquad b = \frac{58}{14} = 4.2" \qquad \text{Use } 6"$$

$$\frac{t}{d} = \frac{3}{14} = .22 \qquad \text{From Plate IX} \qquad \text{T. \& M.}$$

$$\frac{M}{bd} = 85 \qquad j = .905$$

$$b = \frac{M}{85 \times 14} = \frac{325000}{85 \times 196} = 19.5"$$

$$j = .905 \qquad jd = .905 \times 14 = 12.7"$$

$$A = \frac{M}{f_s\ jd} = \frac{325000}{15000 \times 12.7} = 1.71^{a}"$$

Use four 3/4" round rods, area 1.77 "

$$u = \frac{V}{\Sigma o \times jd} = \frac{5800}{(2.36 \times 4) \times 12.7} = 48.3\#^{o}" \qquad \text{Safe in bond stress}$$

$$v = \frac{5800}{6 \times 14} = 69\#^{o}" \qquad \text{Concrete takes } 40\#$$

69 - 40 = 29#°" to be taken by steel.

$$S = \frac{d}{4} = \frac{14}{4} = 3\text{-}1/2" \text{ spacing } 4".$$

$$P = V\ b\ s$$

$$P = 29 \times 6 \times 4 = 700\#$$

$A = \frac{700}{I2000} = .059^{\square"}$

Use I/4" round U bars, spacing 4", starting at point 5'-6" to support. Turn up one horizontal bar 2' from center and one 6'.

Roof Girder Span I6'-8"

$M = \frac{I3I40 \times \overline{I6.7}^{2} \times I2}{I0} = 263500"\#$

$M = \frac{I2-I/2 \times 6 \times I50 \times \overline{I6.7}^{2} \times I2}{I44 \times 8} = 32700"\#$

Total $M = 263500 + 32700 = 296200"\#$

$V = \frac{I3I40}{2} + \frac{I2-I/2 \times 6 \times I50 \times I6.7}{I44 \times 2} = 7I72\#$

$b\,d = \frac{7I72}{I00} = 72 \qquad d = I4" \qquad b = \frac{72}{I4} = 5.34" \qquad$ Use 6"

$\frac{t}{d} = \frac{3}{I4} = .22 \qquad \frac{M}{bd} = 85 \qquad j = .905$

$b = \frac{296000}{85 \times I96} = I7.8"$

$jd = .905 \times I4 = I2.7"$

$A = \frac{296000}{I5000 \times I2.7} = I.55^{\square"}$

Use three 7/8" round rods, area $I.803.^{\square"}$

$u = \frac{7I72}{2.75 \times 3 \times I2.7} = 68.3\#^{\square"}$

$v = \frac{7I72}{6 \times I4} = 85.5\#$

$v = 85.5\# - 40 = 45.5\#$ shear to be carried by steel.

$P = v\,b\,s = 45.5 \times 6 \times 4\text{-}I/2 = I230\#^{\square"}$

$A = \frac{I230}{I2000} = .I025^{\square"}$

Use I/4" round U bars, spacing 4'-6" from center.

Wall Roof Girder. Span I6'-8".

$$M = \frac{5800 \times \overline{I6.7}^2 \times I2}{5} = 233000"\#$$

$$M \text{ due to weight of beam} = \frac{I0 \times I8 \times I50 \times \overline{I6.7}^2 \times I2}{I44 \times 8} = 78500"\#$$

Total M = 233000 + 78500 = 3II500"#

$$d = \frac{3II500}{I0 \times 97.5} = 320 \qquad d = I7.9" \qquad \text{Use } I8"$$

$$A = \frac{M}{f_s jd} = \frac{3II500}{I5000 \times .875 \times I8} = I.32"$$

Use three 3/4" round rods, area I.33^{a}".

$$V = \frac{5800}{2} = \frac{I0 \times I8 \times I50 \times I6.7}{I44 \times 2} = 4465\#$$

$$u = \frac{4465}{I0 \times I8} = 24.8\#^{a}"$$

$$u = \frac{4465}{3 \times 2.36 \times .875 \times I8} = 40\#^{a}"$$

Wall Roof Girder. Span 20'.

$$M = \frac{69.5 \times 4.2 \times 400 \times I2}{I0} = I40000"\#$$

$$M = \frac{I0 \times I6 \times I50 \times 20 \times I2}{I44 \times 8} = I00000"\#$$

Total M = I40000 + I00000 = 240000"#

$$\frac{M}{bd^2} = 97.5 \qquad d^2 = \frac{240000}{I0 \times 97.5} = 246 \qquad d = I5.7"$$

Use I0" x I6" girder.

$$A = \frac{240000}{I5000 \times 7/8 \times I6} = I.I5^{a}"$$

Use two 7/8" round rods, area I.20^{a}".

$$v = \frac{69.5 \times 4 \times 20}{2} = 2920\#$$

$$v = \frac{2920}{10 \times 16} = 18.3\#^{a}"$$

$$u = \frac{2920}{2 \times 2.75 \times .875 \times 16} = 38\#^{a}"$$

FLOOR SLAB.

Exterior Slab. (8'-4" x 20'-0").

Live Load	100#^a"
4" Slab	50
Cement Finish	10
Total Load	160#^a"

$$M = \frac{W L^2}{10} \quad \frac{160 \times \overline{8.33}^{2} \times 12}{10} = 13350"\#$$

$$d^2 = \frac{6 \times 13350}{600 \times 12} = 11.13 \qquad d = 3.34" \qquad \text{Use 4" slab.}$$

$$A = \frac{M}{f_s \times .875 \times d} = \frac{13350}{15000 \times .875 \times 3.25} = .306^{a}"$$

Use 3/8" round rods, spacing 4".

$$V = \frac{8.33 \times 160}{2} = 667\#$$

$$v = \frac{667}{12 \times 4} = 13\#^{a}"$$

$$u = \frac{V}{\Sigma o \; jd} = \frac{667}{(3 \times 1.18) .875 \times 3.25} = 66.3\#^{a}"$$

Interior Slab.

Same thickness as exterior Slab.

$$M = \frac{W L^2}{12} = 1113 0"\#$$

$$A = \frac{1113 0}{15000 \times .875 \times .325} = .26^{a}"$$

Use 3/8" round rods, spacing 4-1/2".

$$U = \frac{V}{\Sigma o\ jd} = \frac{667}{3.15 \times .875 \times 3.25} = 74\#/"$$

Use 3/8" round rods, spacing 4" same as exterior slab to take care of bond stress.

FLOOR BEAM.

End Beam — Span 20'.

$$M = \frac{W\ b\ L^2}{10} = \frac{160 \times 8.33 \times \overline{20}^2 \times 12}{10} = 641000"\#$$

$$\text{B.M. due to weight of beam} = \frac{15-1/2 \times 9 \times 150 \times \overline{20}^2 \times 12}{144 \times 8} = 71800"\#$$

Total M = 641000 + 71800 = 712800"#

$$V = \frac{20 \times 8.33 \times 160}{2} = 13350\#$$

$$db = \frac{13350}{100} = 133.5$$

b = 8.33" Use 9"

$$\frac{t}{d} = \frac{4}{18} = .222 \qquad \frac{M}{bd^2} = 85 \qquad j = .90$$

$$b = \frac{71800}{85 \times 256} = .33"$$

jd = .90 x 18 = 16.2"

$$A = \frac{712800}{15000 \times 16.2} = 2.94/"$$

Use five 7/8" round rods, area 3.03/".

$$U = \frac{V}{\Sigma o \times jd} \quad \frac{13350}{(5 \times 2.75) \times 16.2} = 60\#/"$$

$$v = \frac{13350}{9 \times 18} = 82.5\#$$

82.5 - 40 = 42.5# carried by vertical rods.

P = v b s = 42.5 x 9 x 6 = 2300#

$$A = \frac{2300}{12000} = .192/"$$

Use 3/8" round U bars, area .22I$^{\square}$", spacing 4" for 2-I/2′ and 6" for 2-I/2′.

Floor Girder. Span I6′-8".

Load (floor reaction)	26700#
Weight of beam	2400
Total Load	29I00#

$$M = \frac{29I00 \times \overline{I6.7}^2 \times I2}{5} = II6800"\#$$

$$M = \frac{I5\text{-}I/2 \times 9 \times I50 \times \overline{I6.7}^2 \times I2}{I44 \times 8} = 60800"\#$$

Total M = II6800 + 60800 = I77600"#

$$V = \frac{29I00 + I45 \times I6.7}{2} = I5760\#$$

$$b\ d = \frac{I5760}{I00} = I57.6$$

Let d = I8" $\quad b = \frac{I57.6}{I8} = 8.75"$ Use 9"

$$\frac{t}{d} = \frac{4}{I8} = .222 \qquad \frac{M}{bd^2} = 85 \qquad j = .90 \qquad jd = .90 \times I8 = I6.2$$

$$b = \frac{I77600}{85 \times 324} = 44.6"$$

$$A = \frac{}{I5000 \times I6.2} = 5.06^{\square}"$$

Use nine 7/8" round rods, area 5.4$^{\square}$".

$$u = \frac{I5760}{2.75 \times 8 \times .90 \times I8} = 45\#^{\square}"$$

$$v = \frac{I5760}{I8 \times 9} = 97.3\#^{\square}"$$

97.3 - 40 = 57.3#$^{\square}$" to be carried by steel.

P = 57.3 x 9 x 4-I/2 = 2320#

$A = \frac{2320}{I2000} = .I97^{a}"$

Use 3/8" round U bars, spacing 4'-I0" from center of span.
Turn up 2 rods, 6' from center of span.

Wall Floor Girder. Span I6'-8".

$M = \frac{I4550 \times \overline{I6.7}^{2} \times I2}{5} = 583000"\#$

$M = \frac{300 \times \overline{I6.7}^{2} \times I2}{8} = I25000"\#$

Total M = 583000 + I25000 = 708000"#

$\frac{M}{bd^{2}} = 98 \qquad d^{2} = \frac{708000}{98 \times I2} \qquad d = 24"$

$A = \frac{708000}{I5000 \times .875 \times 24} = 2.II^{a}"$

Use three I" round rods.

$V = \frac{I4550 \times 300 \times I6.7}{2} = 9780\#$

$v = \frac{9780}{I2 \times 24} = 34\#^{a}"$

$u = \frac{9780}{3 \times 3.I4 \times .875 \times 24} = 44\#^{a}"$

Use I2" x 24" girder.

Wall Floor Girder. Span 20'.

Weight of Brick = $\frac{I3 \times I \times 3 \times I44}{I2} = 468\#$ per ft.

Floor Load = 667# per ft.

W = 468 + 667 = II35# per ft.

$M = \frac{W L^{2}}{I0} = \frac{II35 \times \overline{20}^{2} \times I2}{I0} = 544800"\#$

$M = \frac{I50 \times 2 \times 400 \times I2}{8} = I80000"\#$

Total M = 544800 + I80000 = 724800"#

$d^2 = \frac{724800}{I2 \times 98} = 6I5$ d = 24" Use I2" x 24" girder.

$A = \frac{724800}{I5000 \times .875 \times 24} = 2.2^{a}"$

Use three I" round rods, area $2.3^{a}"$.

$V = \frac{II35 \times 20}{2} = II350\#$

$v = \frac{II350}{I2 \times 24} = 39.5\#^{a}"$ $40\#^{a}"$ allowable.

$u = \frac{II350}{9.43 \times .875 \times 24} = 58\#^{a}"$

INTERIOR COLUMNS.

Fourth Floor.

Slab & Roofing	20 x I6.7 x 69.5	23200#
One Girder	$\frac{I2\text{-}I/2 \times 6 \times I50 \times I6.7}{I44}$	I305
Two Beams	$\frac{I2\text{-}I/2 \times 6 \times I50 \times I6.7}{I44}$	3I30
Assume Column	II" x II"	I390
Total Load		29025#

Let P = I.5%

P = f A (I - (n - I) p) = 400 x A (I - (I5 - I) .0I5)'

An II" x II" column allows I-I/2" for fireproofing.

Steel area = .0I5 x 60 = $.90^{a}"$.

Use four 9/I6" round rods, area $I.00^{a}"$.

Third Floor.

Roof Load	29025#
Fourth Floor Cement Finish	3340
" " 4" Slab	I6700

One Floor Girder	2430
Two " Beams	5820
Assume I6" x I6" Column	2940
85% Live Load Fourth Floor	28390
Total Load	88645#

Let P = 2%

$88645 = 400 \times A\ (I - (I5 - I)\ .02)$

$A = \frac{88645}{400 \times I.28} = I72^{\square}"$ b = I3"

A I6" x I6" column allows I-I/2" for fireproofing.

Steel area = $.02 \times I72 = 3.44^{\square}"$.

Use eight 3/4" round rods, area $3.53^{\square}"$.

Second Floor.

Roof Load	29025#
Fourth Floor Load	59620
Third Floor Dead Load	3I230
80% Live Load	26700
Assume 20" x 20" Column	4580
Total Load	I5II55#

Let P = 2.5%

$I5II55 = 400 \times A\ (I - (I5 - I)\ .025)$

$A = \frac{I5II55}{540} = 280^{\square}"$ b = I6.75"

A 20" x 20" column allows I-I/2" for fireproofing.

Steel area = $.025 \times 280 = 7.0^{\square}"$

Use nine I" round rods, area $7.07^{\square}"$.

First Floor.

Loading above Second Floor	I5II55#
Second Floor Loading	3I230
75% Live Load	25070
Assume 22-I/2" x 22-I/2" Column	5820
Total Load	2I3275#

Let P = 3%

$2I3275 = 400 \times A\ (I - (I5 - I)\ .03)$

$A = \frac{2I3275}{400 \times I.42} = 383^{a}"$ $\quad b = I9.5"$

A 22-I/2" x 22-I/2" column allows I-I/2" for fireproofing.

Steel area $= .03 \times 384 = II.52^{a}"$.

Use nine I-3/8" round rods, area $I3.3^{a}"$.

Basement.

Loading above First Floor	2I3275#
First Floor Dead Load	3I230
70% Live Load	23380
Assume Column 26" x 26"	7050
Total Load	274935#

Let P = 3%

$274935 = 400 \times A\ (I - (I5 - I)\ .03)$

$A = \frac{274935}{400 \times I.42} = 484^{a}"$ $\quad b = 22"$

A 25" x 25" column allows I-I/2" for fireproofing.

Steel area $= .03 \times 484 = I4.52^{a}"$.

Use ten I-3/8" round rods, area $I4.85^{a}"$.

Interior Column Footing.

Load = 274935# Column = 25" x 25"

5000# sq.ft. = allowable bearing pressure.

Load on Footing	274935#
Assume Weight of Footing	25000
Total Load	299935#

$\frac{299935}{5000}$ = 60 sq.ft. Use 7'-9" x 7'-9" footing.

$\frac{274935}{40 \times 4 \times 25}$ = 68.75" Dept of footing = 5'-9"

Shear reinforcing in footing short direction.

500 x 2.08 x 2.833 = 29500#

M = 29500 x I.4 = 4I300"#

$A = \frac{4I300 \times I2}{I5000 \times .875 \times 65} = .58"$

Use 5/8" round rods, spacing 6".

Shear reinforcing in footing diagonal direction.

5000 x 2.625 x 2.625 = 34500#

M = 34500 x 3.7I x I2 = I540000"#

$A = \frac{I540000}{I5000 \times .875 \times 65} = I.8^{a}"$

Use six 5/8" round ords, area $I.85^{a}$".

WALLS COLUMNS SpAN 20'

Fourth Floor.

Roof Slab and Load	II600#
One 20ft. Beam I0" x I6"	3330
One I6'-8" Beam I2-I/2" x 6"	I320
One half 20 ft Beam I2-I/2" x 6"	780

30" Paraput Wall I2"	6000
II" x II" Column	I290
Total Load	24320#

P = I.5%

$A = \frac{24320}{484} = 50.2^{a}"$ b = 7"

A II" x II" column is the minimum size allowable.

Steel area = .0I5 x 50.2 = $.75^{a}"$

Use four I/2" round rods, area $.80^{a}"$.

Tie rods every I2" with I/8" wire.

Third Floor.

4" Slab and Floor Finish	I0020#
One 20' Beam I2" x 24"	6000
One-half 20 Floor Beam I5-I/2" x 9"	I455
One I6'-8" Floor Girder I5-I/2" x 9"	2430
Brick Masonry	8000
One-half Panel of 85% Live Load	I4200
I4-I/2" x I4-I/2" Column	2200
Load from Fourth Floor Column	24320
Total Load	68625#

P = 2%

$A = \frac{68625}{5I2} = I34^{a}"$ b = II.5"

A I4-I/2" x I4-I/2" column allows I-I/2" for fireproofing.

Steel area = .02 x I4.5 = $2.90^{a}"$.

Use five 7/8" round rods, area $3.0^{a}"$.

Tie rods every I2" with I/8" wire.

Second Floor.

Load from Third Floor Column	68625#
Third Floor Dead Load	27905
One-half Panel of 80% Live Load	I3350
I7-I/2" x I7-I/2" Column	3200
Total Load	II3080#

P = 2.5%

$A = \frac{II3080}{540} = 209^{a}"$ b = I4.5 + 3 = I7.5"

A I7-I/2" x I7-I/2" column allows I-I/2" for fireproofing.

Steel area = .025 x 209 = $5.23^{a}"$.

Use nine 7/8" round rods, area $5.4^{a}"$.

Tie rods every I2" with I/8" wire.

First Floor.

Load from Second Floor Column	II3080#
Second Floor Dead Load	27905
One-half Panel 75% Live Load	I2535
20" x 20" Column	4I80
Total Load	I57700#

P = 3.0%

$A = \frac{I57700}{568} = 278^{a}"$ b = I6.7"

A 20" x 20" column allows I-I/2" for fireproofing.

Steel area = .03 x 278 = $8.34^{a}"$.

Use seven I-I/4" round rods, area $8.4^{a}"$.

Basement.

Load from Forst Floor Column	I57700#
First Floor Dead Load	27905
One-half Panel of 70% Live Load	II690
22" x 22" Column	4580
Total Load	20I875#

P = 3%

$A = \frac{20I875}{568} = 356''$" b = I8.9"

A 22" x 22" column allows I-I/2" for fireproofing.

Steel area = .03 x 356 = I0.68"

Use nine I-I/4" round rods, area II.0448".

Tie rods every I2" with I/8" wire.

Wall Column Footing.

Load on Footing	20I875#
Weight of Footing	20000
Total Load	22I875#

Area of base $= \frac{22I875}{5000} = 44.48''$' b = 6'-8"

$\frac{20I875}{40 \times 4 \times 22} = 57.4$" Make depth of footing 5'-0".

Shear reinforcing in short direction.

5000 x I.83 x 2.43 = 22300#

M = 22300 x I.25 = 27900 #

$A = \frac{27900 \times I2}{I5000 \times .875 \times 56} = .46''$"

Use three I/2" round rods.

Shear reinforcing in diagonal direction.

$5000 \times 2.43 \times 2.43 = 29500\#$

$M = 29500 \times 2.9I = 85800"\#$

$$A = \frac{85800 \times I2}{I5000 \times .875 \times 56} = I.4^{a}"$$

WALL COLUMNS SPAN I6'-8"

Fourth Floor.

Roof Slab and Load	II600#
One Wall Girder I0" x I8"	3I40
Two Roof Beams I2-I/2" x 6"	2640
30" Paraput Wall I2"	5000
II" x II" Column	I290
Total Load	23670#

$P = I.5\%$

$$A = \frac{23670}{484} = 49.0^{a}" \qquad b = 7"$$

An II" x II" column is the minimum size allowable.

Steel area $= .0I5 \times 49 = .735^{a}"$.

Use four I/2" round rods, area .80".

Tie rods every I2" with I/8" wire.

Third Floor.

Load from Fourth Floor Column	23670#
One Wall Girder I2" x 24"	5000
Two Floor Beams I5-I/2" x 9"	4860
One-half Slab and Floor Finish	I0020
Brick Masonry	6800
One-half Panel of 85% Live Load	I4200
I4-I/2" x I4-I/2" Column	2200
Total Load	66740#

P = 2%

$A = \frac{66740}{512} = 130^{\square}"$ b = 11.4"

A 14-1/2" x 14-1/2" column allows 1-1/2" for fireproofing.

Steel area = .02 x 130 = $2.6^{\square}"$.

Use six 3/4" round rods, area $2.6508^{\square}"$.

Tie rods every 12" with 1/8" wire.

Second Floor.

Load from Third Floor Column	66740#
Third Floor Dead Load	26680
One-half Panel of 80% Live Load	13350
17-1/2" x 17-1/2" Column	3200
Total Load	109970#

P = 2.5%

$A = \frac{109970}{540} = 204^{\square}"$ b = 14.3"

A 17-1/2" x 17-1/2" column allows 1-1/2" for fireproofing.

Steel area = .025 x 204 = $5.1^{\square}"$.

Use nine 7/8" round rods, area $5.4^{\square}"$.

Tie rods every 12" with 1/8" wire.

First Floor.

Load from Second Floor Column	109970#
Second Floor Dead Load	26680
One-half Panel of 75% Live Load	12535
20" x 20" Column	4180
Total Load	153365#

P = 3%

$A = \frac{153365}{568} = 270^{\square}"$ $\quad b = 16.4"$

A 20" x 20" column allows 1-1/2" for fireproofing.

Steel area $= .03 \times 270 = 8.1^{\square}"$.

Use seven 1-1/4" round rods, area $8.4^{\square}"$.

Tie rods every 12" with 1/8" wire.

Basement.

Load from First Floor Column	153365#
First Floor Dead Load	26680
One-half Panel of 70% Live Load	11690
22" x 22" Column	4580
Total Load	196315#

P = 3%

$A = \frac{196315}{568} = 346^{\square}"$ $\quad b = 18.6"$

A 22" x 22" column allows 1-1/2" for fireproofing.

Steel area $= .03 \times 346 = 10.38^{\square}"$.

Use nine 1-1/4" round rods, area $11.0^{\square}"$.

Tie rods every 12" with 1/8" wire.

RAFT FOOTING.

Load on Interior Column	274935#
" " Wall "	196315
Weight of Footing	80000
Pressure on Soil	501250#

$A = \frac{501250}{5000} = 100.25$

$\frac{6 + 3}{2} \times 22.5 = 101.5$

$\frac{47I250}{40 \times I66} = 72"$ depth of footing.

The raft footing is considered as a beam; the span being the distance between the two columns; the load the upward reaction of the earth. It is designed as an inverted T-beam.

$W = 5000 \times 4\text{-}I/2" = 22500\#$

$M = \frac{22500 \times \overline{20}^{2} \times I2}{I0} = I0,800,000"\#$

$V = \frac{22500 \times 20}{2} = 225000\#$

$\frac{22500}{I33} = I700$

$b\ d = I700 \qquad d = 68" \qquad b = \frac{I700}{68} = 25"$

$\frac{t}{d} = \frac{8}{68} = .II8 \qquad \frac{M}{bd^2} = 56 \qquad j = .95$

$b = \frac{I0,800,000}{56 \times (68)^2} = 42"$

$A = \frac{I0,800,000}{I5000 \times .95 \times 68} = II.2^{a}"$

Use twelve I-I/8" round rods.

Bond stress.

$u = \frac{224000}{(I2 \times 3.54)\ .95 \times 68} = 80\#^{a}"$

Shear.

$v = \frac{225000}{68 \times 25} = I33\#^{a}"$

I33 - 40 = 93# to be taken by U bars.

$\frac{d}{4} = \frac{68}{4} = I7"$ spacing.

$p = 93 \times 68 \times I7 = I07500\#$

$\frac{I07500}{I2000} = .90^{a}"$

Use 3/4" U bars, spacing I7".

DESIGN OF STAIRWAY.

Width of Stairs.

$72 = (15000 - 3000)\ 6 = 144" = 12'$

Two 24" Stairway Fire-escapes $= 4'$

Width of Stairs $= 8'$

Stairway is designed with two rectangular beams as strings supporting a 4" slab with risers and treads.

Distance between floors = 10'-0".

Use 15 risers at 8" and 14 treads at 12".

Design of 4" Slab.

Live Load	100# "
Weight of Slab	50
Total Load	150# "

$$M = \frac{150 \times 8^2 \times 12}{10} = 11530"\#$$

$$d^2 = \frac{11530}{600 \times 12} = 9.60 \qquad d = 3.1$$

A 4" slab is ample.

$$A = \frac{11530}{15000 \times .875 \times 3} = .30^{\square"}$$

Use 1/2" round rods, spacing 6", area $.392^{\square"}$

$$V = \frac{150 \times 8}{2} = 600^{\#}$$

$$U = \frac{600}{3.14 \times .875 \times 3} = 73\#^{\square"} \qquad \frac{600}{4 \times 12} = 12.5\#^{\square"} \qquad 40" \text{ allowable}$$

Design of Rectangular Beam.

Live Load = 100 x 4 =	400#
Concrete	300
Total Load	700#

M due to weight of beam $= \frac{300 \times \overline{14}^2 \times 12}{8} = 88200\#$

Total M = 164500 + 88200 = 252700"#

$\frac{M}{bd^2} = 98 \qquad d^2 = \frac{252700}{98 \times 10} = 225 \qquad d = 15$

Use a 10" x 15" beam.

$A = \frac{252700}{15000 \times .875 \times 13.5} = 1.43^{\square}"$

Use four 3/4" round bars, area $1.76^{\square}"$.

$V = \frac{700 \times 14}{2} = 4900\#$

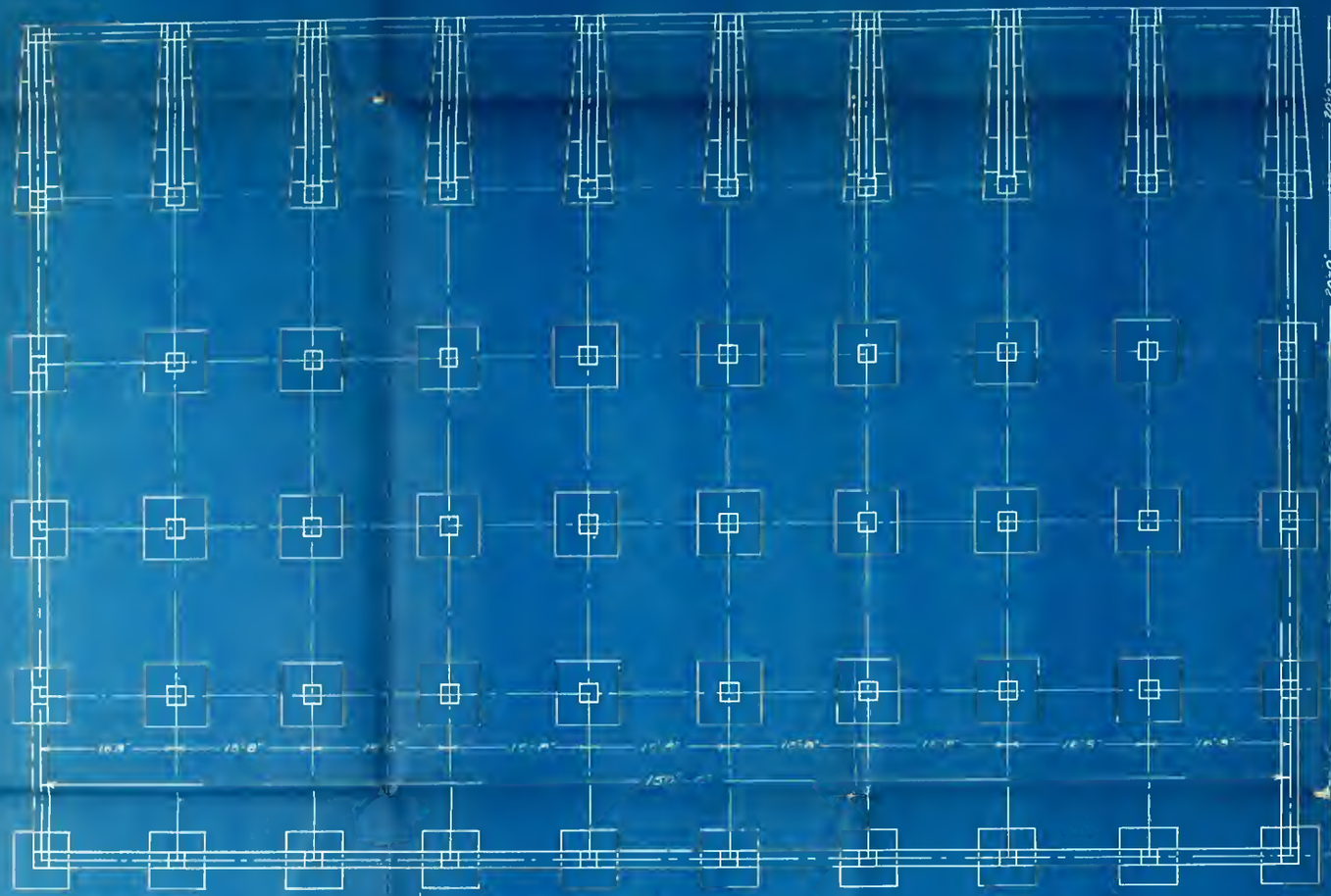
$U = \frac{4900}{4 \times 2.36 \times .875 \times 13.5} = 44\#/"$

$u = \frac{4900}{10 \times 15} = 33\#/"$

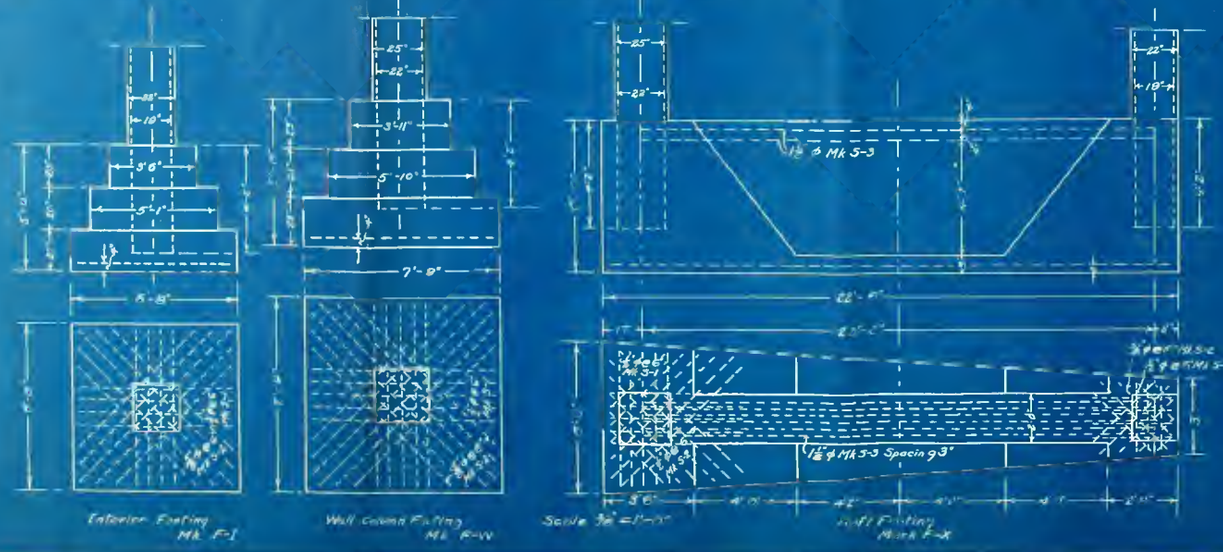
No shears bars are required.

PLANS.

PLAN OF FOOTINGS Scale 1/8"=1'-0"



Scale 1/8"=1'-0"



Schedule of Columns

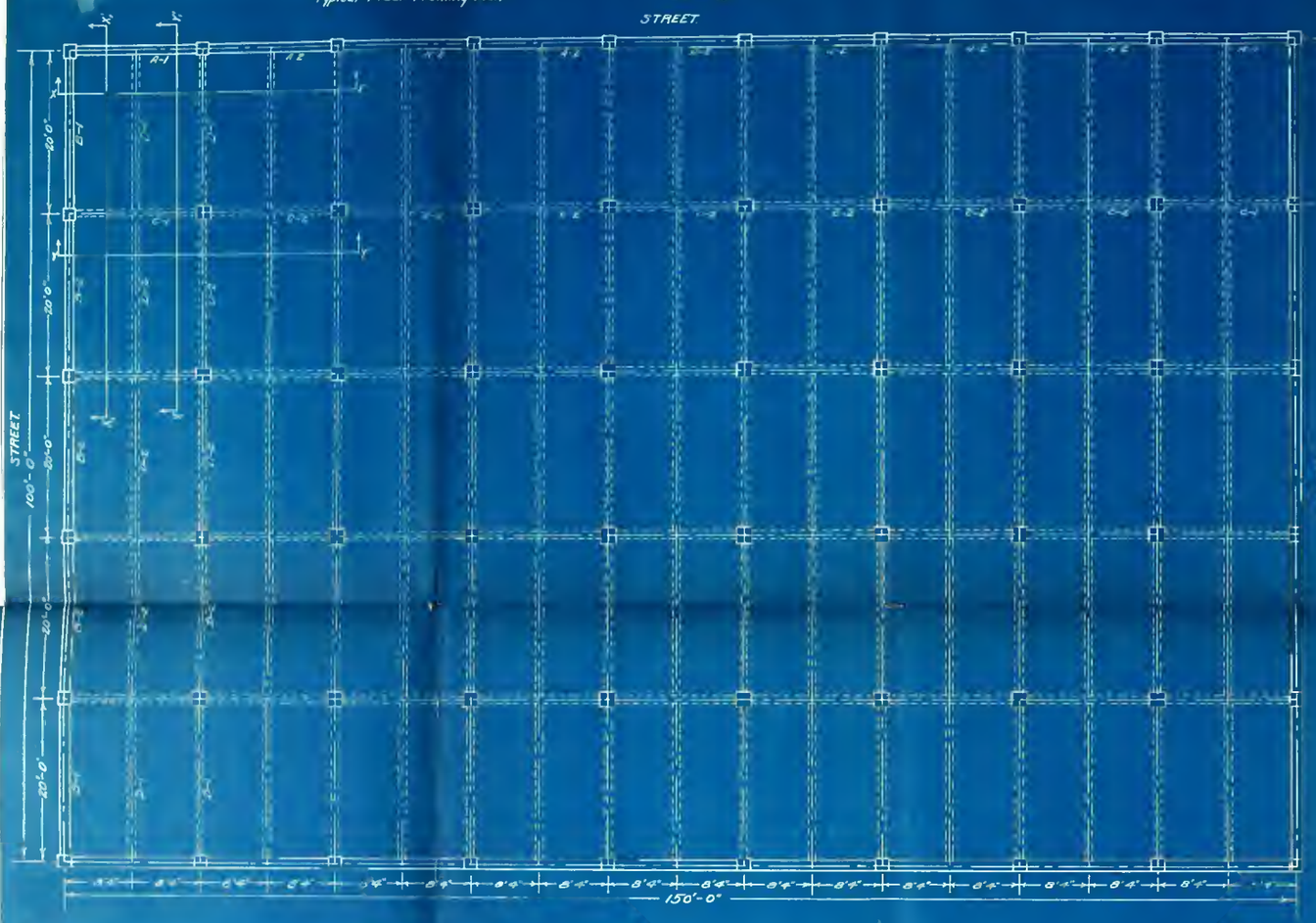
Mark	Number	Size	Steel	Remark
I-4	32	11"X11"X11'-0"	4-3/8" ϕ Length 13'-0"	All vertical reinforcement
I-3	32	16"X16"X11'-0"	8-3/4" ϕ " 15'-0"	in columns tied with
I-2	32	20"X20"X11'-0"	9-1" ϕ " 15'-0"	1/4" wire every 12"
I-1	32	22½"X22½"X11'-0"	8-1 3/8" ϕ " 15'-0"	
I-B	32	25"X25"X10'-0"	10-1 3/8" ϕ " 16'-0"	
W-4	28	18"X10"X11'-0"	4-1/2" ϕ " 13'-0"	
W-3	28	18"X12"X11'-0"	5 7/8" ϕ " 15'-0"	
W-2	28	18"X17"X11'-0"	8-3/4" ϕ " 15'-0"	
W-1	28	18"X22"X11'-0"	7-1 1/2" ϕ " 15'-0"	
W-B	28	22"X22"X10'-0"	9-1 3/4" ϕ " 16'-0"	

Schedule of Footings

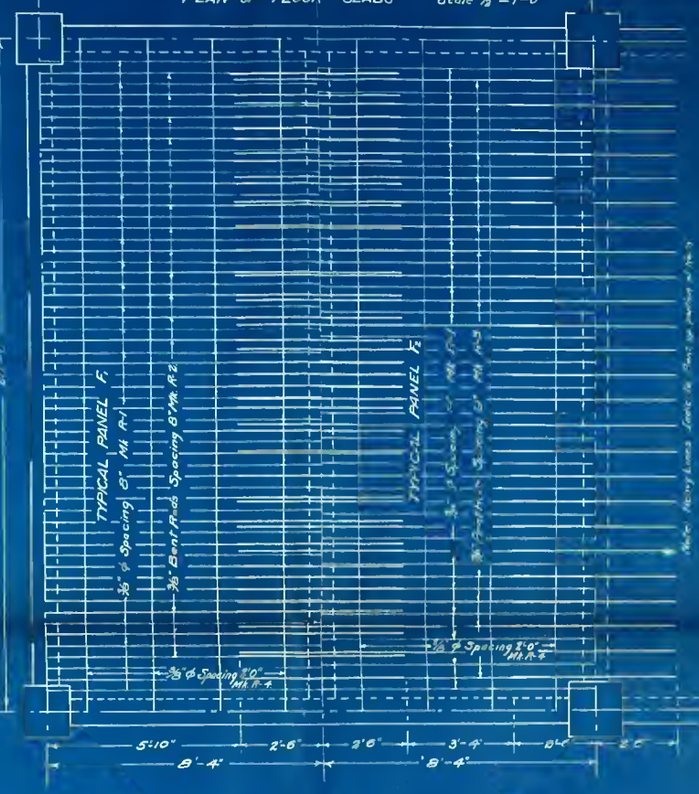
Mark	Number	Steel Mark S-1	Steel Mark S-2	Steel Mark S-3
F-I	24	8-1/2" ϕ Length 6'-0"	10-5/8" ϕ Length 8'-0"	
F-W	16	10-1/2" ϕ " 7'-0"	12-5/8" ϕ " 12'-0"	
F-X	10	8-1/2" ϕ " 3'-0"	10-5/8" ϕ " 14'-0"	12-1 1/2" ϕ Length 21'-0"
"	"	10-1/2" ϕ " 4'-0"	12-5/8" ϕ " 6'-0"	

ARMOUR INSTITUTE OF TECHNOLOGY
CIVIL ENGINEERING DEPARTMENT
PLANS OF A FOUR-STORY
REINFORCED CONCRETE BUILDING
Scale as indicated May 1913
Thesis Plate I
C.A. Leibrandt

Typical Floor Framing Plan Scale 1/8"=1'-0"

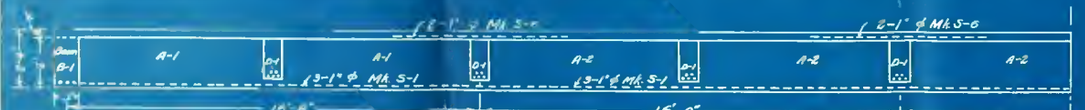


PLAN OF FLOOR SLABS Scale 1/8"=1'-0"



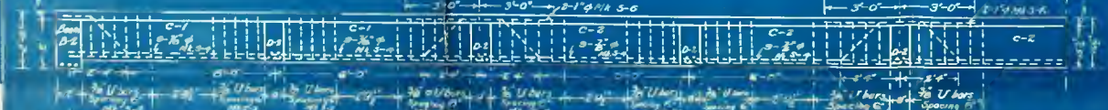
Schedule of Floor Slab Steel

Slab	No. per Floor	Steel
F	10	28 - 3/8" ϕ Mk-A-1 Length 8'-4"
"	"	28 3/8" Bent bars " A-2 " 10'-10"
"	"	6 - 3/8" ϕ " A-4 " 20'-0"
F1	80	26 - 3/8" ϕ " A-1 " 8'-4"
"	"	20 - 3/8" Bent bars " A-3 " 13'-4"
"	"	4 - 3/8" ϕ " A-1 " 20'-0"

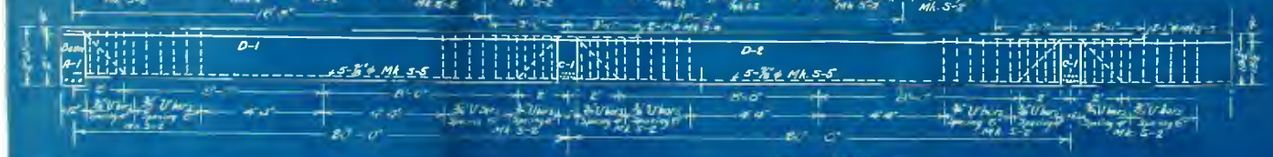


Section Thru X-X

Section Thru X-X



Section Thru Y-Y



Section Thru Y-Y

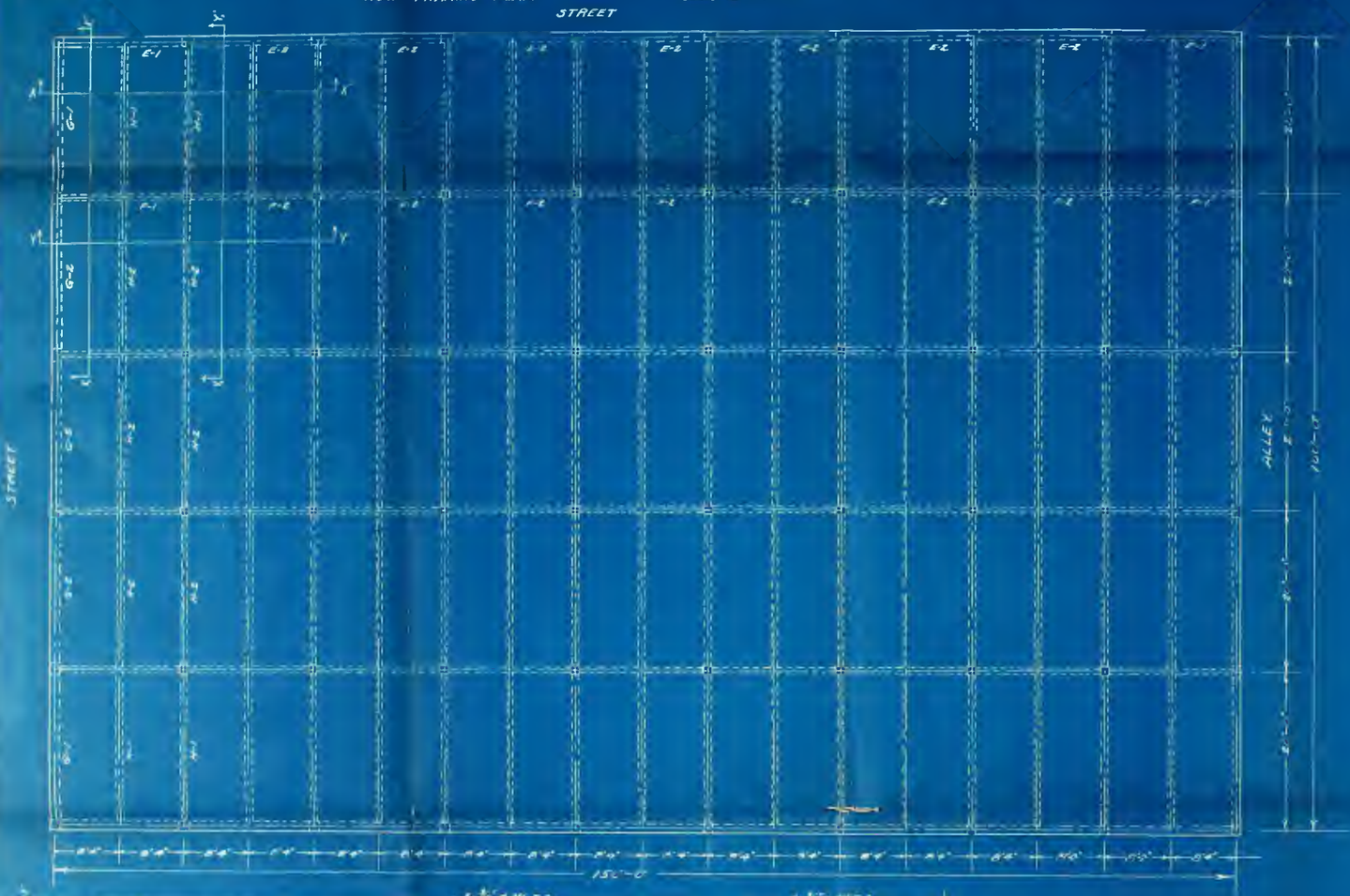
Scale 3/8"=1'-0"

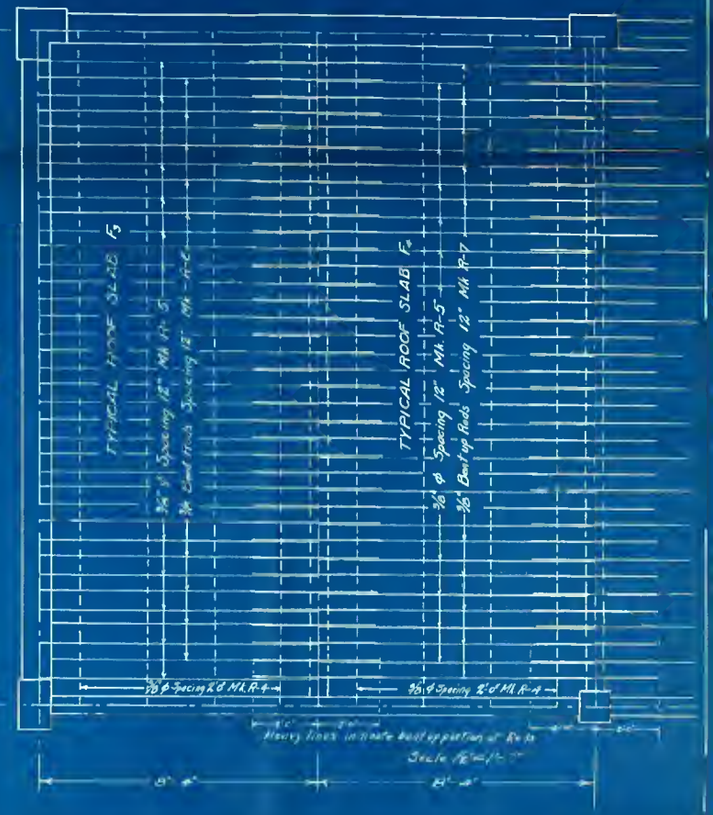
SCHEDULE OF BEAMS

MARK	SIZE	LENGTH	No. per Floor	STEEL
A-1	12"X24"	16'-0"	4	3-1" ϕ Mk S-1 Length 16'-8"
				2-1" ϕ " S-6 " 5'-0"
B-1	12"X24"	20'-0"	4	3-1" ϕ " S-3 " 20'-0"
				2-1" ϕ " S-6 " 6'-0"
C-1	9"X18½"	16'-8"	8	9-⅞" ϕ " S-4 " 16'-8"
				2-1" ϕ " S-6 " 6'-0"
				22-⅜" U bars " S-2 6"X14"
D-1	9"X15½"	20'-0"	30	5-⅞" ϕ " S-5 Length 20'-0"
				2-1" ϕ " S-6 " 6'-0"
				22-⅜" U bars " S-2 6"X14"
A-2	12"X24"	16'-8"	14	3-1" ϕ Mk S-1 Length 16'-8"
				2-1" ϕ " S-6 " 6'-0"
B-2	12"X24"	20'-0"	6	3-1" ϕ " S-3 " 20'-0"
				2-1" ϕ " S-6 " 6'-0"
C-2	9"X15½"	16'-8"	28	9-⅞" ϕ " S-4 " 16'-8"
				2-1" ϕ " S-6 " 6'-0"
				22-⅜" U bars " S-2 6"X14"
D-2	9"X15½"	20'-0"	51	5-⅞" ϕ " S-5 Length 20'-0"
				2-1" ϕ " S-6 " 6'-0"
				22-⅜" U bars " S-2 6"X14"

ARMOUR INSTITUTE OF TECHNOLOGY
CIVIL ENGINEERING DEPARTMENT
PLANS OF A FLOUR-STORY
REINFORCED CONCRETE BUILDING
Scale as indicated May 1913
Thesis Plate 2
C.A. Leiferman Jr.

ROOF FRAMING PLAN. Scale 1/8" = 1'-0"





SCHEDULE OF ROOF-SLAB STEEL

SLAB	No. Required	STEEL
F_3	10	19-3/8" ϕ Mk R-5 Length 8'-4"
		18-3/8" Bent Rods Mk R-6 " 10'-4"
		4-3/8" ϕ Mk R-4 " 20'-0"
F_4	80	10-3/8" ϕ Mk R-5 " 8'-4"
		19-3/8" Bent Rods Mk R-7 " 12'-4"
		4-3/8" ϕ Mk R-4 " 20'-0"

SCHEDULE OF ROOF BEAMS

MARK	SIZE	LENGTH	NO REQ	STEEL
E-1	10"X16"	16'-0"	18	3-3/4" ϕ Mk T-2 Length 16'-0"
				2-3/4" ϕ Mk T-3 " 8'-0"
G-1	10X18	20'-0"	10	2-7/8" ϕ Mk T-4 " 20'-0"
				2-3/4" ϕ " T-3 " 8'-0"
F-1	6"X12½"	16'-8"	36	3-7/8" ϕ " T-6 " 16'-8"
				2-7/8" ϕ " T-3 " 8'-0"
				34-½" U bars Mk T-1
H-1	6X12½	20'-0"	85	4-3/4" ϕ Mk T-5 " 20'-0"
				2-3/4" ϕ Mk T-3 " 8'-0"
				26-½" U bars Mk T-1

Illinois Institute of Technology
Civil Engineering Department
Plans of a Four-Story
Reinforced Concrete Building
Scale as indicated May 1913
Thesis Plate 3
O.R. Wilmarth